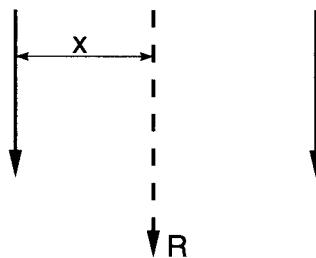


# FACITLISTE

## 1. KRÆFTER OG MOMENTER

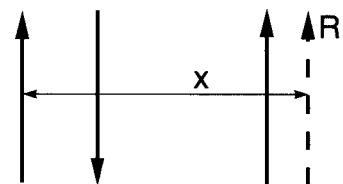
1.  $H = 86,99 \text{ N}$ ,  $V = 96,61 \text{ N}$
2.  $R = 100 \text{ N}$ ,  $v = 53,13^\circ$
3.  $R = 338,54 \text{ N}$ ,  $v = 22,01^\circ$
4.  $F = 17,32 \text{ N}$
5.  $F_{AC} = 400 \text{ N}$ ,  $F_{BC} = 300 \text{ N}$
6.  $R = 861,25 \text{ N}$ ,  $v = -6,41^\circ$
7.  $F_1 = F_2 = 1,3 \text{ kN}$
8. Højre ben:  $F = 544,5 \text{ N}$ , Venstre ben:  $F = 189,1 \text{ N}$
9.  $H = 1 \text{ kN}$ ,  $V = 1,73 \text{ kN}$
10. a)  $F_1 = F_2 = 0,5 \text{ kN}$   
b)  $F_1 = F_2 = 0,54 \text{ kN}$   
c)  $F_1 = F_2 = 0,71 \text{ kN}$   
d)  $F_1 = F_2 = 1 \text{ kN}$   
e)  $F_1 = F_2 = 1,93 \text{ kN}$
11.  $F_1 = 704,98 \text{ N}$ ,  $F_2 = 328,74 \text{ N}$
12.  $R = 7794 \text{ N}$  ( $g = 10 \text{ m/s}^2$ )
13.  $R = 600 \text{ N}$
14.  $R = 1,17 \text{ kN}$ ,  $v = 13,28^\circ$
15.  $R = 1189 \text{ N}$ ,  $v = 32,54^\circ$
16.  $R = 23,58 \text{ N}$ ,  $v = 354,57^\circ$
17.  $R = 660,69 \text{ N}$ ,  $v = 202,88^\circ$
18.  $R = 440,69 \text{ N}$ ,  $v = 4,38^\circ$

19.  $R = 5,51 \text{ MN}$ ,  $v = 337,6^\circ$
20.  $R = 21,26 \text{ kN}$
21.  $R = 35 \text{ N}$ ,  $x = 1,97 \text{ m}$



ad. 21

22.  $R = 12 \text{ N}$ ,  $x = 4,17 \text{ m}$



ad. 22

23.  $R = 14,7 \text{ MN}$

$x = 4,13$

$v = 85^\circ$

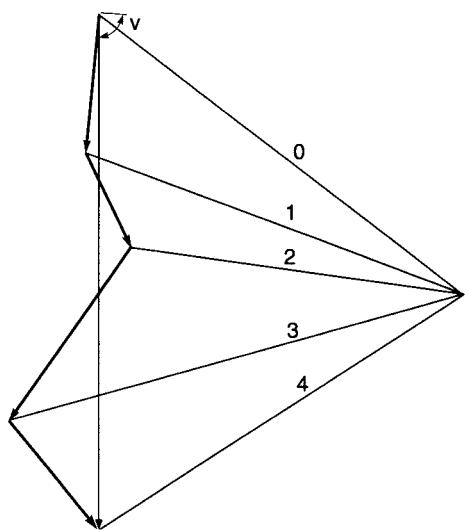
24.  $M_A = 22 \text{ kNm}$

25.  $M_A = 16004 \text{ Nmm}$

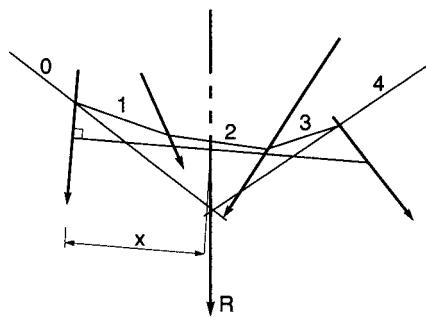
26.  $M_A = 106 \text{ Nm}$

27.  $M_A = 9,068 \text{ kNm}$

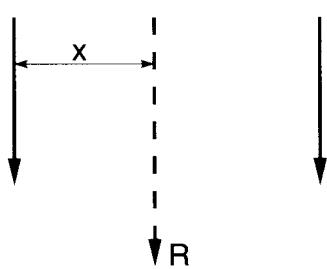
28. a)  $F_1 = F_2 = 7,78 \text{ kN}$   
b)  $M_A = 178,76 \text{ kNm}$



ad. 23

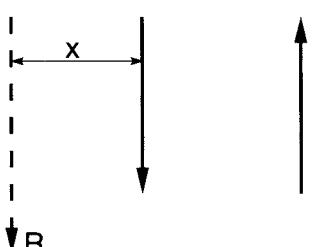


29.  $R = 43 \text{ MN}$        $x = 1,47 \text{ m}$



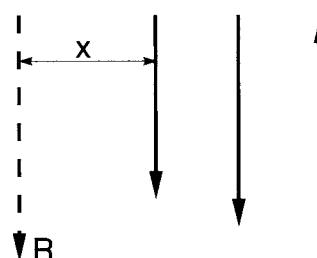
ad. 29

30.  $R = 13 \text{ kN}$        $x = 1,14 \text{ m}$



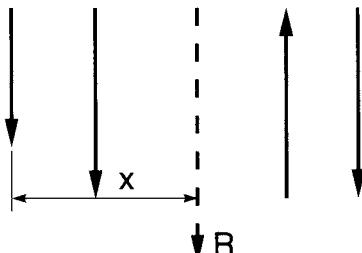
ad. 30

31.  $R = 10 \text{ N}$        $x = 11 \text{ m}$



ad. 31

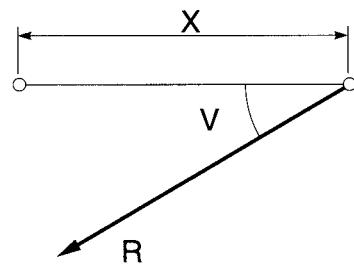
32.  $R = 41 \text{ N}$        $x = 2,3 \text{ m}$



ad. 32

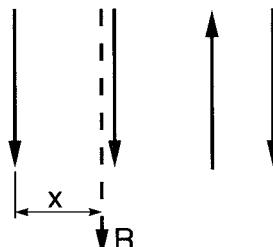
33.  $R = 90 \text{ N}$        $M_A = 500 \text{ Nm}$

34.  $x = 1,5 \text{ m}$   
 $R = 5,57 \text{ kN}$   
 $v = 21,04^\circ$



ad. 34

35.  $R = 7 \text{ kN}$        $x = 7,36 \text{ m}$

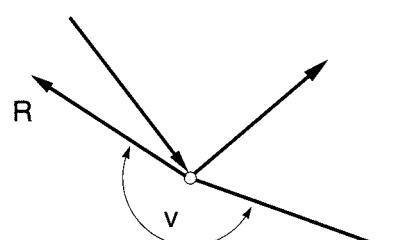


ad. 35

36.  $R = 373,44 \text{ N}$  ( $R_V = 3616 \text{ N}$ ,  $R_H = 93,3 \text{ N}$ )  
 $(x,y) = (0,96, -11,6)$

37.  $F_1 = 80 \text{ N}$

38.  $R = 2,57 \text{ MN}$        $v = 182^\circ$



ad. 38

39.  $F_2 = 2,33 \text{ kN}$

40.  $F = 0,49 \text{ kN}$

41.  $F_1 = 1091 \text{ N}$

42. a)  $F_2 = 765 \text{ N}$   
 b)  $F_1 = 392 \text{ N}$

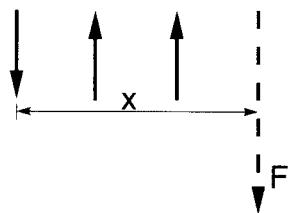
43.  $a_1 = 102 \text{ mm}$

44.  $F_1 = 217 \text{ N}$

45.  $F_2 = 700 \text{ N}$

46.  $F = 12,5 \text{ N}$

47.  $\downarrow F = 20 \text{ N}$        $x = 9,5 \text{ m}$



ad. 47

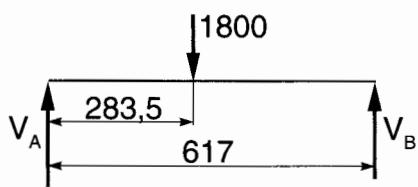
48.  $F = 386 \text{ N}$

49.  $A = 3,29 \text{ kN}$        $B = 3,71 \text{ kN}$

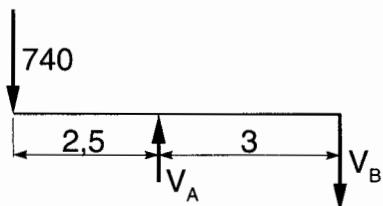
50. a)  $F = 1,04 \text{ kN}$   
b)  $A = 1,41 \text{ kN}$        $B = 2,45 \text{ kN}$

## 2. KONSTRUKTIONER PÅVIRKET TIL BØJNING

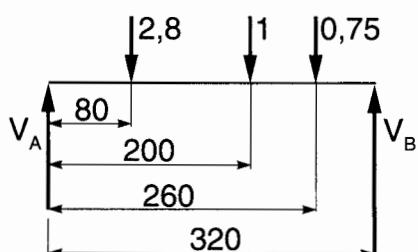
51.  $V_A = 973 \text{ N}$   
 $V_B = 827 \text{ N}$



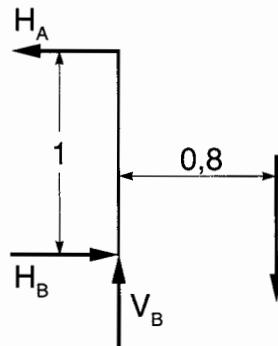
52.  $V_A = 1357 \text{ N}$   
 $V_B = 617 \text{ N}$



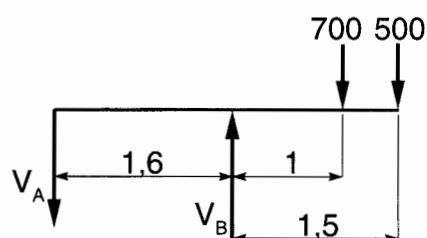
53.  $V_A = 2,62 \text{ kN}$   
 $V_B = 1,93 \text{ kN}$



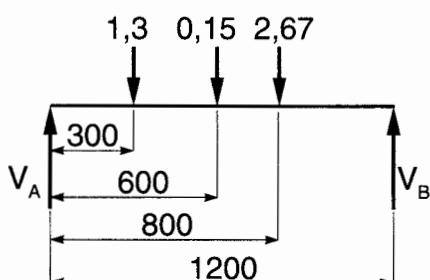
54.  $H_A = 400 \text{ N}$   
 $H_B = 400 \text{ N}$   
 $V_B = 500 \text{ N}$



55.  $V_A = 906 \text{ N}$   
 $V_B = 2106 \text{ N}$

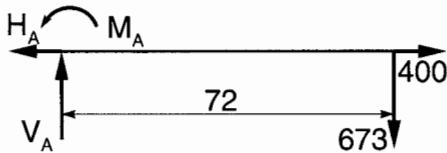


56.  $V_A = 1,94 \text{ kN}$   
 $V_B = 2,18 \text{ kN}$

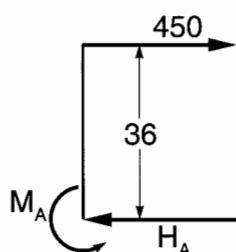


57.  $F_2 = 2,25 \text{ KN}$

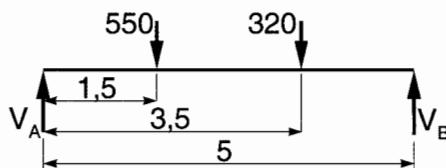
58.  $H_A = 400 \text{ N}$   
 $V_A = 693 \text{ N}$   
 $M_A = 49896 \text{ Nmm}$



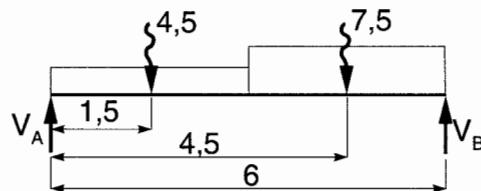
59.  $H_A = 450 \text{ N}$   
 $M_A = 11700 \text{ Nmm}$



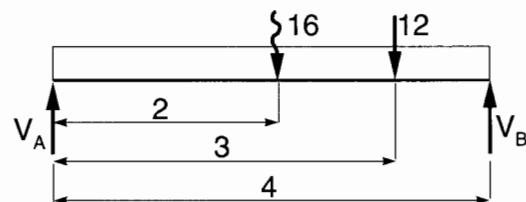
- 60a.  $H_A = 0$   
 $V_A = 481 \text{ N}$   
 $V_B = 389 \text{ N}$



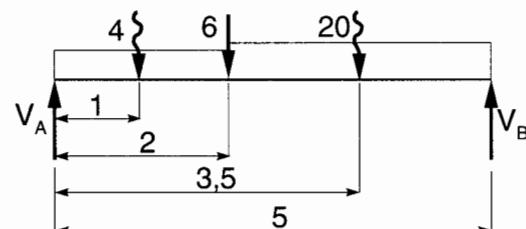
- 60b.  $H_B = 0$   
 $V_A = 5,25 \text{ kN}$   
 $V_B = 6,75 \text{ kN}$



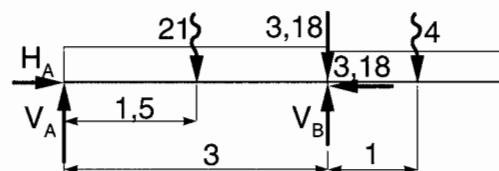
- 60c.  $H_A = 0$   
 $V_A = 11 \text{ kN}$   
 $V_B = 17 \text{ kN}$



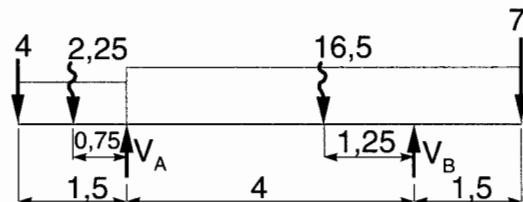
- 60d.  $H_A = 0$   
 $V_A = 12,8 \text{ kN}$   
 $V_B = 17,2 \text{ kN}$



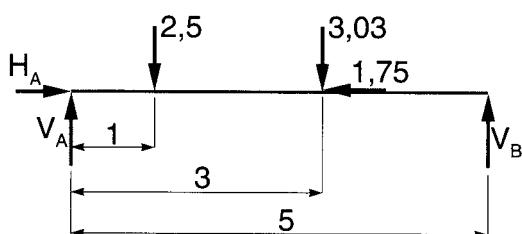
- 60e.  $H_A = 3,18 \text{ kN}$   
 $V_A = 9,17 \text{ kN}$   
 $V_B = 19,02 \text{ kN}$



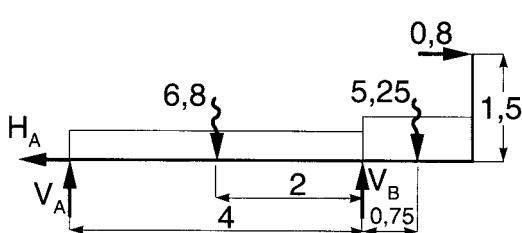
- 60f.  $H_A = 0$   
 $V_A = 10,7 \text{ kN}$   
 $V_B = 19,05 \text{ kN}$



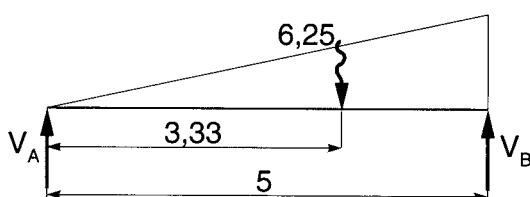
60g.  $H_A = 1,75 \text{ kN}$   
 $V_A = 3,21 \text{ kN}$   
 $V_B = 2,32 \text{ kN}$



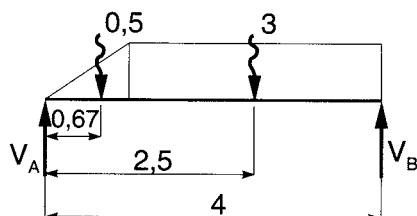
60h.  $H_A = 0,8 \text{ kN}$   
 $V_A = 2,12 \text{ kN}$   
 $V_B = 9,93 \text{ kN}$



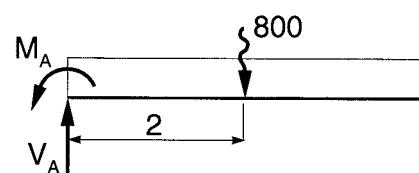
60i.  $H_A = 0$   
 $V_A = 2,08 \text{ kN}$   
 $V_B = 4,17 \text{ kN}$



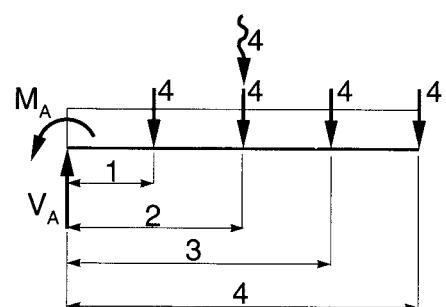
60j.  $H_A = 0$   
 $V_A = 1,54 \text{ kN}$   
 $V_B = 1,96 \text{ kN}$



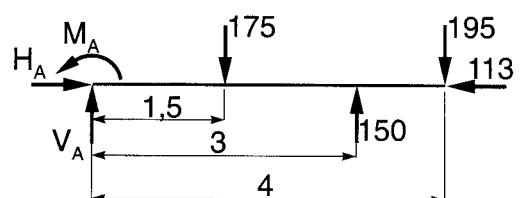
61a.  $V_A = 800 \text{ kN}$   
 $M_A = 1600 \text{ kNm}$



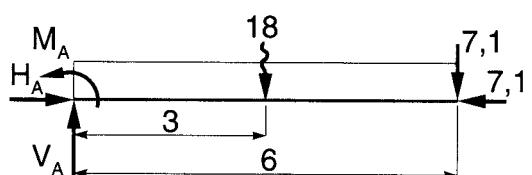
61b.  $V_A = 20 \text{ kN}$   
 $M_A = 48 \text{ kNm}$



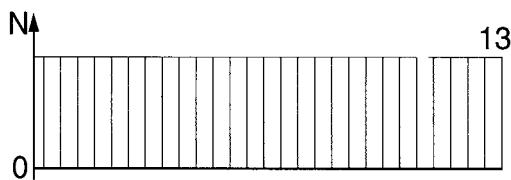
61c.  $H_A = 113 \text{ N}$   
 $V_A = 220 \text{ N}$   
 $M_A = 592,5 \text{ Nm}$



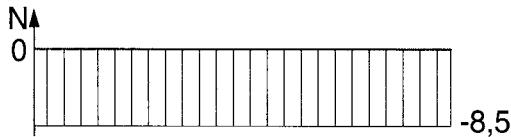
61d.  $V_A = 25,1 \text{ kN}$   
 $H_A = 7,1 \text{ kN}$   
 $M_A = 96,6 \text{ kNm}$



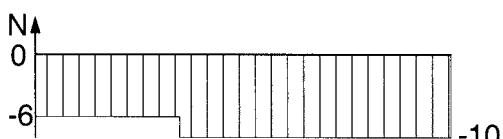
62. a)  $N_{AB} = 13 \text{ kN}$



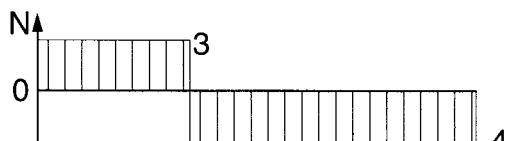
63. a)  $N_{AB} = -8,5 \text{ kN}$



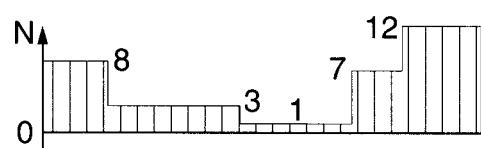
64. a)  $F_C = 10 \text{ kN}$   
b)  $N_{AB} = -6 \text{ kN}$   
 $N_{BC} = -10 \text{ kN}$



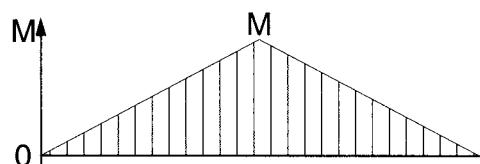
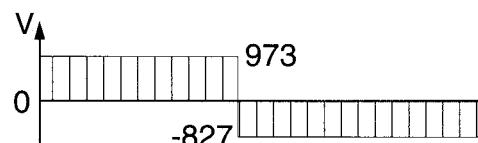
65. a)  $F_C = 4 \text{ kN}$   
b)  $N_{AB} = 3 \text{ kN}$   
 $N_{BC} = -4 \text{ kN}$



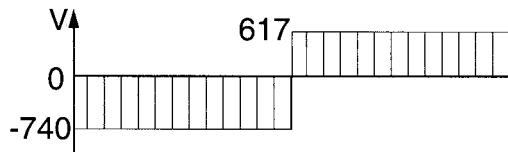
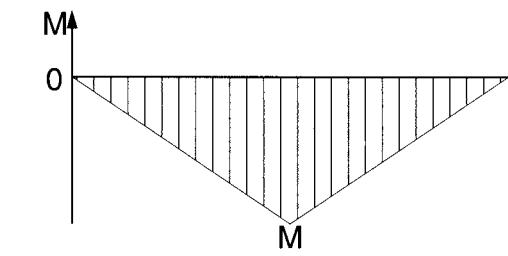
66. a)  $F_F = -12 \text{ kN}$   
b)  $N_{AB} = 8 \text{ kN}$   
 $N_{BC} = 3 \text{ kN}$   
 $N_{CD} = 1 \text{ kN}$   
 $N_{DE} = 7 \text{ kN}$   
 $N_{EF} = 12 \text{ kN}$



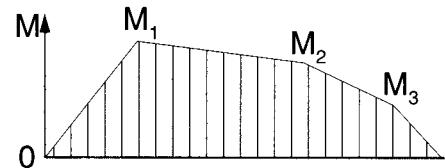
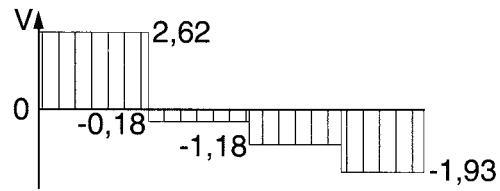
67.  $M = 275845,5 \text{ Nmm}$



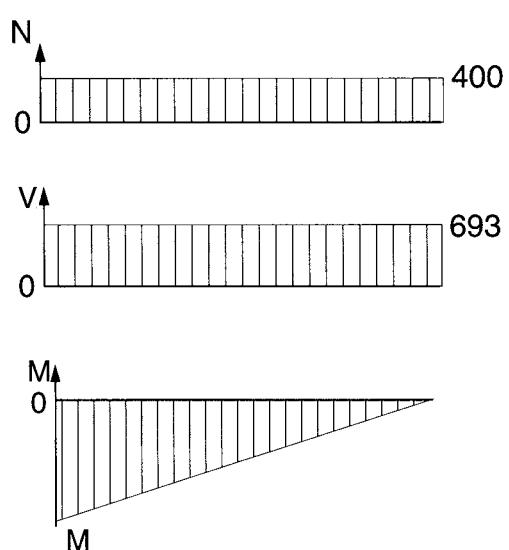
68.  $M = -1850 \text{ Nm}$



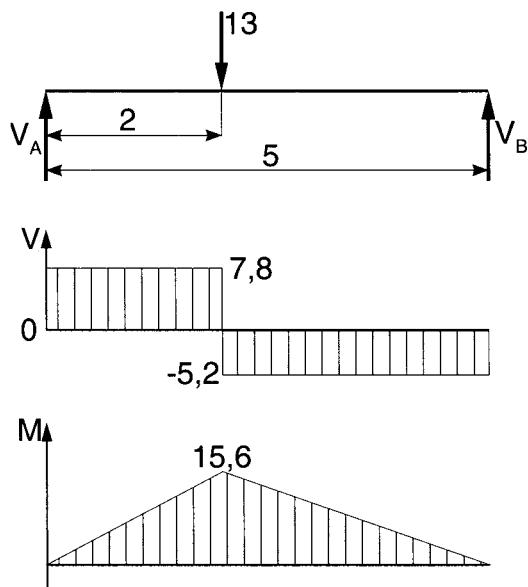
69.  $M_1 = 2,096 \text{ kNm}$   
 $M_2 = 1,88 \text{ kNm}$   
 $M_3 = 1,158 \text{ kNm}$



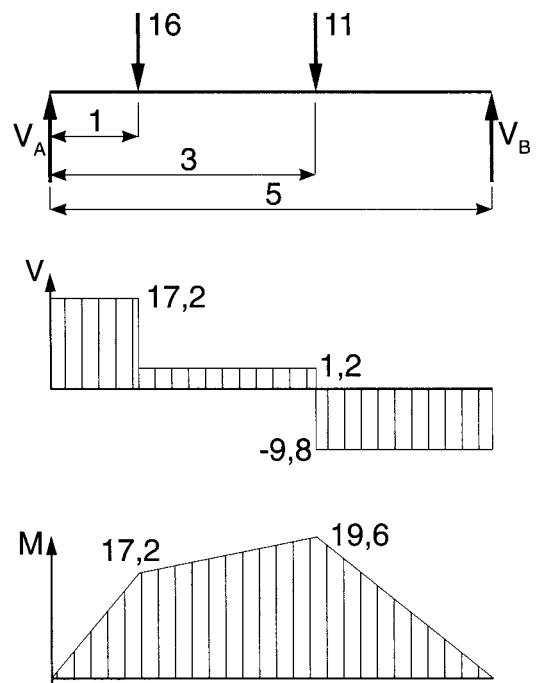
70.  $M = 49896 \text{ Nmm}$



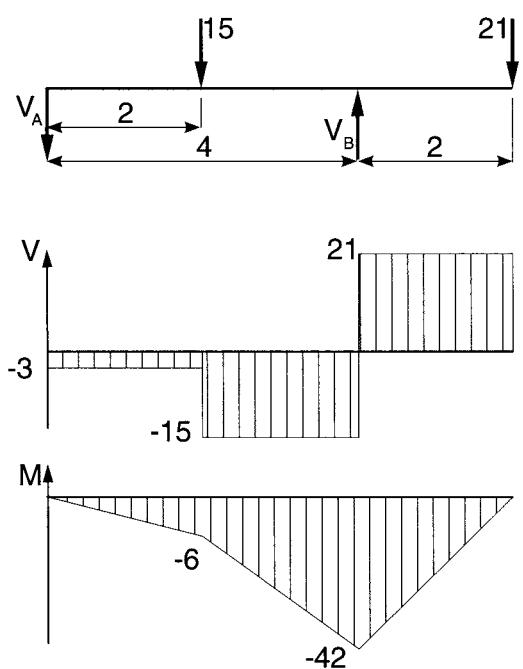
71a.  $V_A = 7,8 \text{ kN}$   
 $V_B = 5,2 \text{ kN}$   
 $M = 15,6 \text{ kNm}$



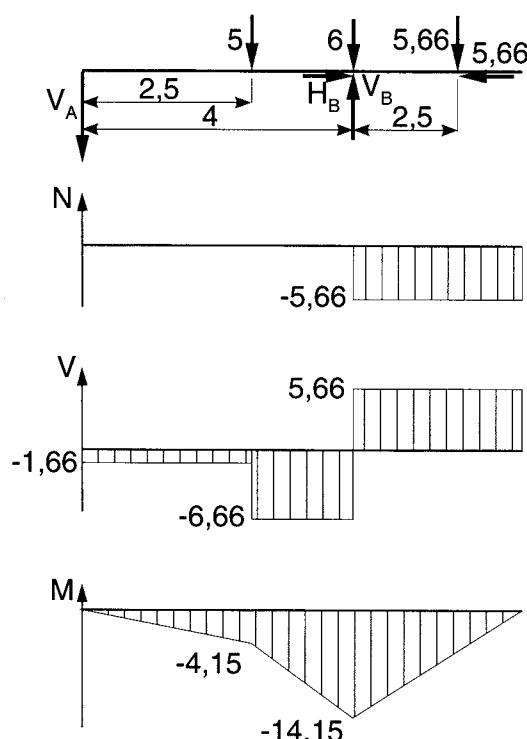
71b.  $V_A = 17,2 \text{ kN}$   
 $V_B = 9,8 \text{ kN}$



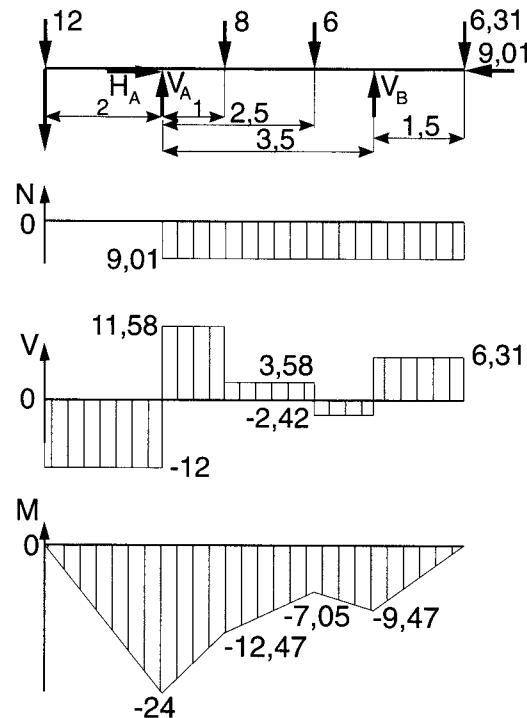
71c.  $V_A = 3 \text{ kN}$   
 $V_B = 39 \text{ kN}$



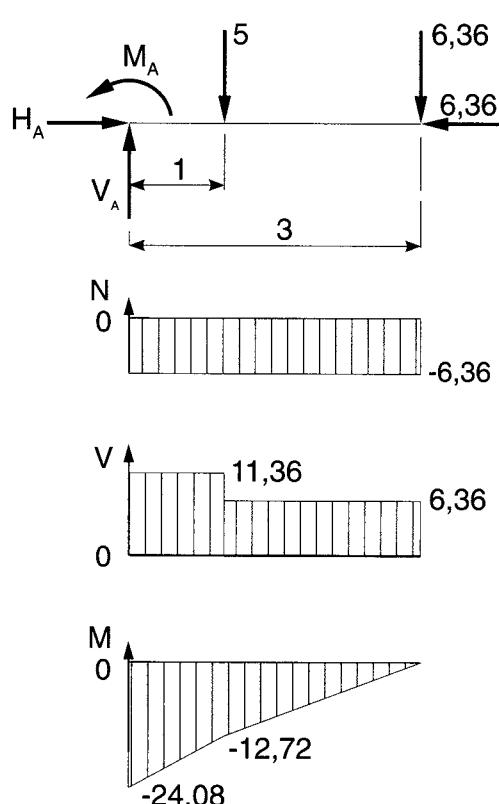
71d.  $V_A = 1,66 \text{ kN}$   
 $V_B = 18,32 \text{ kN}$   
 $H_B = 5,66 \text{ kN}$



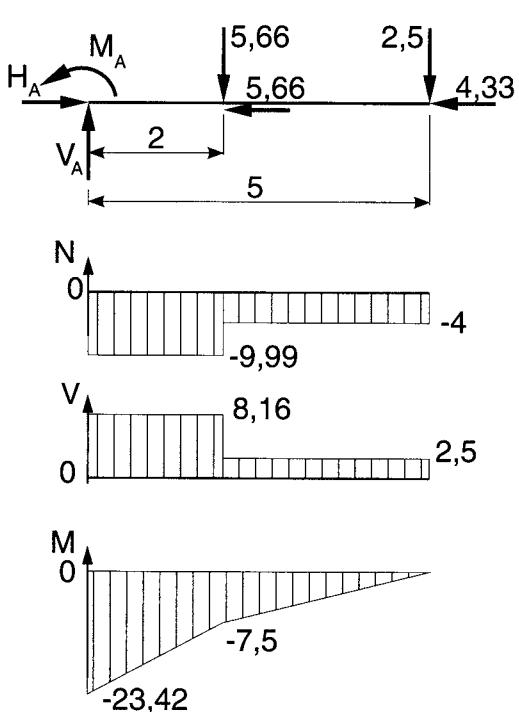
71e.  $H_A = 9,01 \text{ N}$   
 $V_A = 23,58 \text{ N}$   
 $V_B = 8,73 \text{ kNm}$



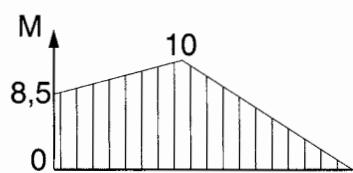
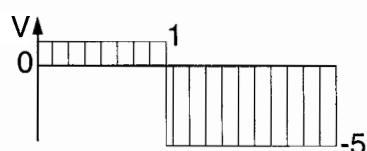
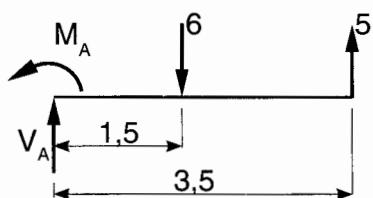
71f.  $H_A = 6,36 \text{ kN}$   
 $V_A = 11,36 \text{ kN}$   
 $M_A = 24,08 \text{ kNm}$



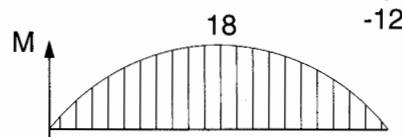
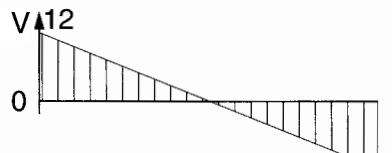
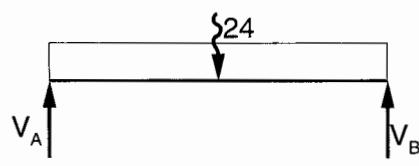
71g.  $H_A = 9,99 \text{ N}$   
 $V_A = 8,16 \text{ N}$   
 $M_A = 23,42 \text{ kNm}$



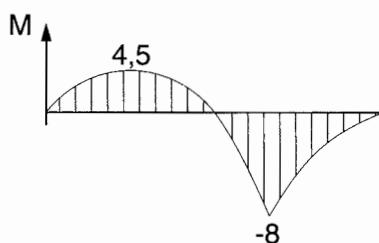
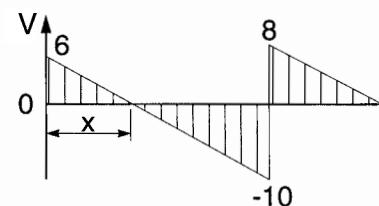
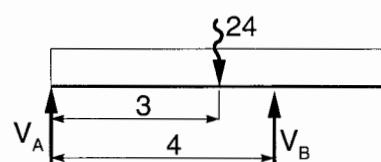
71h.  $V_A = 1 \text{ MN}$   
 $M_A = 8,5 \text{ MNm}$



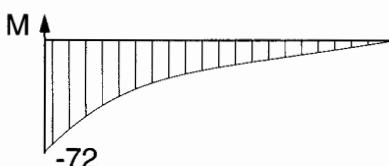
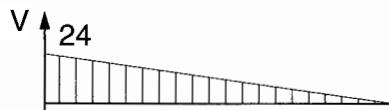
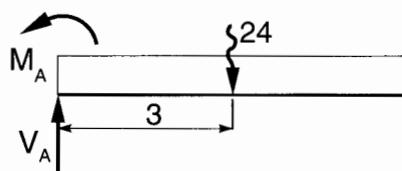
72a.  $V_A = V_B = 12 \text{ kN}$   
 $M = 18 \text{ kNm}$

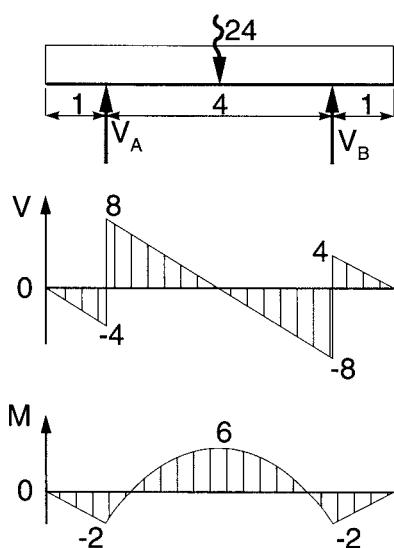
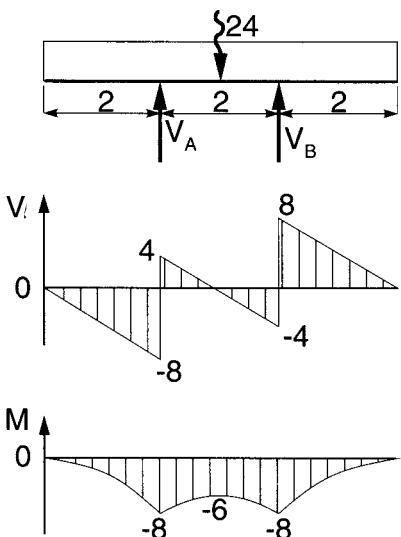


72b.  $V_A = 6 \text{ kN}$   
 $V_B = 18 \text{ kN}$   
 $x = 1,5 \text{ m}$



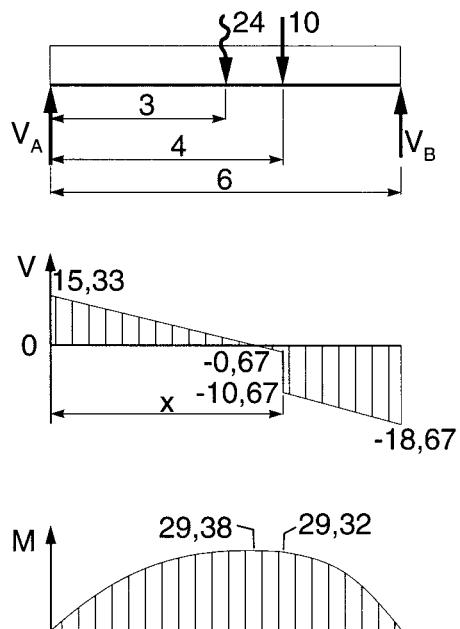
72c.  $V_A = 24 \text{ kN}$   
 $M_A = 72 \text{ kNm}$



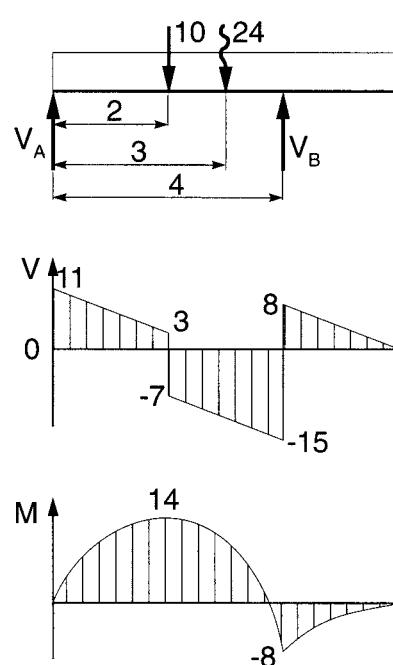
72d.  $V_A = V_B = 12 \text{ kN}$ 72e.  $V_A = V_B = 12 \text{ kN}$ 72f.  $V_A = 15,33 \text{ kN}$ 

$$V_B = 18,67 \text{ kN}$$

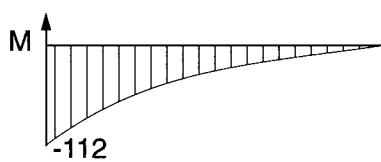
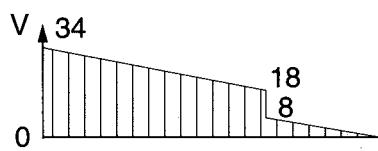
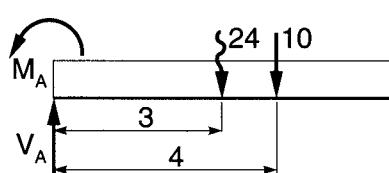
$$x = 3,83 \text{ m}$$

72g.  $V_A = 11 \text{ kN}$ 

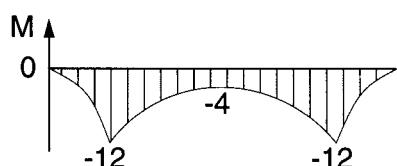
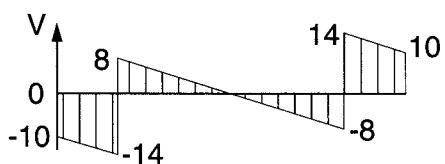
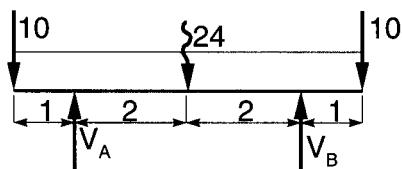
$$V_B = 23 \text{ kN}$$



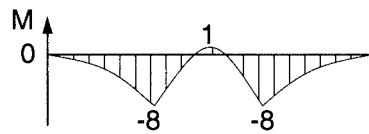
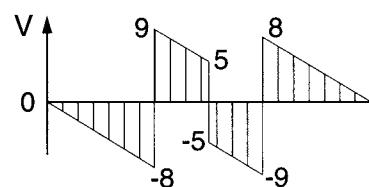
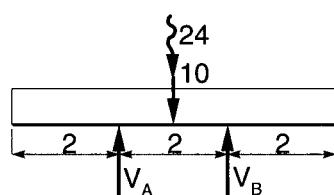
72h.  $V_A = 34 \text{ kN}$   
 $M_A = 112 \text{ kNm}$



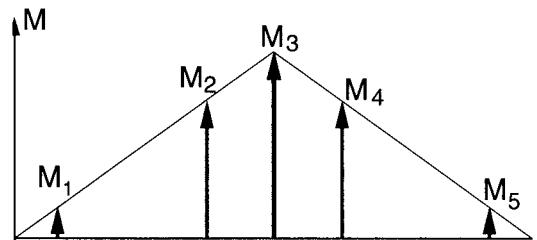
72i.  $V_A = V_B = 22 \text{ kN}$



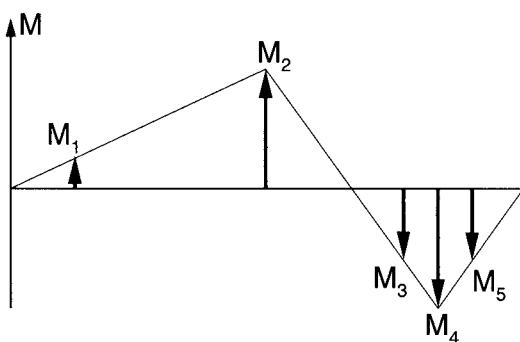
72j.  $V_A = V_B = 17 \text{ kN}$



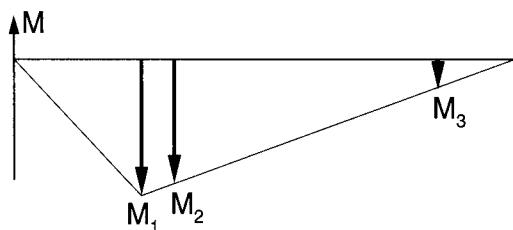
73. a)  $V_A = 11,69 \text{ kN}$   
 $V_B = 10,31 \text{ kN}$   
 b)  $M_1 = 187,04 \text{ kNm}$   
 $M_2 = 1262,52 \text{ kNm}$   
 $M_3 = 1753,5 \text{ kNm}$   
 $M_4 = 1299,06 \text{ kNm}$   
 $M_5 = 164,96 \text{ kNm}$



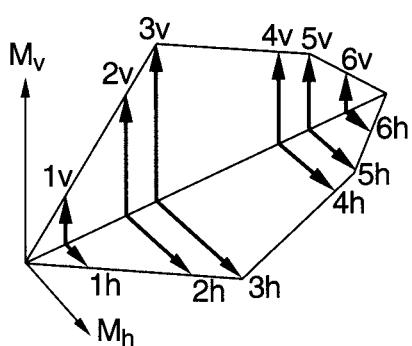
74. a)  $V_A = 0,8 \text{ kN}$   
 $V_B = 8,7 \text{ kN}$   
 b)  $M_1 = 24 \text{ kNm}$   
 $M_2 = 224 \text{ kNm}$   
 $M_3 = -190 \text{ kNm}$   
 $M_4 = -328 \text{ kNm}$   
 $M_5 = -205 \text{ kNm}$



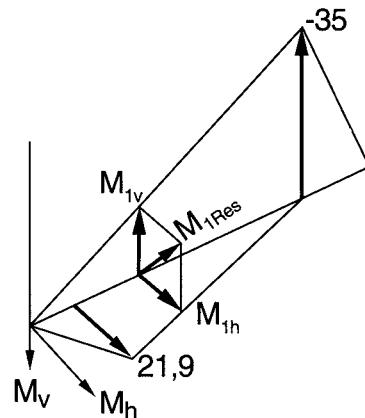
75. a)  $V_A = 28,8 \text{ kN}$   
 $V_B = 4,8 \text{ kN} (\downarrow)$   
 b)  $M_1 = -1920 \text{ kNm}$   
 $M_2 = -1824 \text{ kNm}$   
 $M_3 = -96 \text{ kNm}$



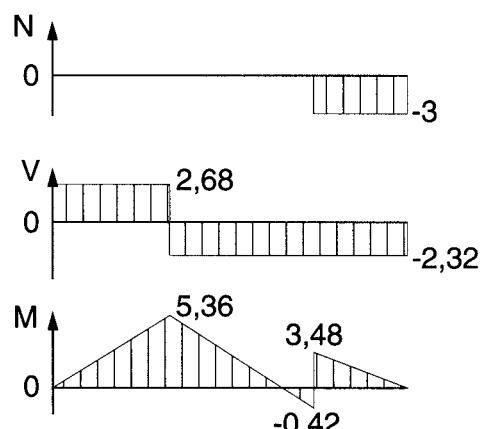
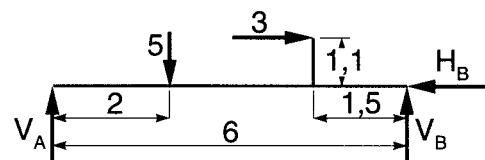
76. a)  $V_A = 12,18 \text{ kN}$   
 $V_B = 12,82 \text{ kN}$   
 $H_A = 9,125 \text{ kN}$   
 $H_B = 8,375 \text{ kN}$   
 c)  $M_{1\text{Res}} = 152,19 \text{ kNm}$   
 $M_{2\text{Res}} = 608,76 \text{ kNm}$   
 $M_{3\text{Res}} = 837,05 \text{ kNm}$   
 $M_{4\text{Res}} = 496,09 \text{ kNm}$   
 $M_{5\text{Res}} = 328,83 \text{ kNm}$   
 $M_{6\text{Res}} = 153,13 \text{ kNm}$



77. a)  $V_A = 0,39 \text{ kN} (\downarrow)$   
 $V_B = 1,79 \text{ kN}$   
 b)  $H_A = 0,73 \text{ kN}$   
 $H_B = 0,37 \text{ kN}$   
 c)  $M_{\text{Res}} = 24,3 \text{ kNm}$



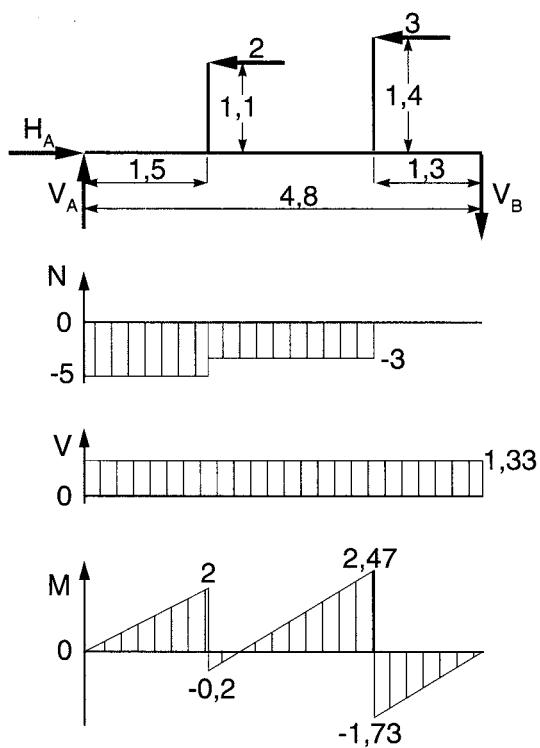
- 78a.  $H_B = 3 \text{ kN}$   
 $V_A = 2,68 \text{ kN}$   
 $V_B = 2,3 \text{ kN}$



78b.  $H_B = 5 \text{ kN}$

$V_A = 1,33 \text{ kN}$

$V_B = 1,33 \text{ kN} (\downarrow)$



### 3. GITTERKONSTRUKTIONER

79.  $H_A = 6 \text{ MN}$

$V_A = 5,625 \text{ MN}$

$V_B = 9,375 \text{ MN}$

80.  $V_A = 0,96 \text{ MN}$

$V_B = 5,54 \text{ MN}$

81.  $H_A = 6,92 \text{ MN}$

$H_B = 6,92 \text{ MN}$

$V_B = 8 \text{ MN}$

82.  $H_A = 298,38 \text{ N}$

$V_A = 19,56 \text{ N}$

$V_B = 139,61 \text{ N} (\downarrow)$

83.  $V_A = 250 \text{ N}$

$V_B = 1050 \text{ N}$

84. a)  $V_A = V_B = 20 \text{ MN}$

b)  $S_1 = -20 \text{ MN}$  (trykstang)

$S_2 = 7,07 \text{ MN}$  (trækstang)

$S_3 = 15 \text{ MN}$  (trækstang)

85. a)  $V_A = V_B = 60 \text{ MN}$

b)  $S_1 = -60 \text{ MN}$  (trykstang)

$S_2 = 21,21 \text{ MN}$  (trækstang)

$S_3 = 45 \text{ MN}$  (trækstang)

86. a)  $H_A = 12 \text{ MN}$

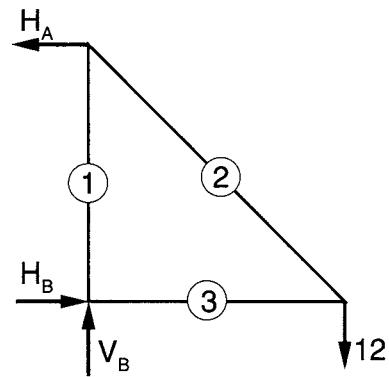
$H_B = 12 \text{ MN}$

$V_B = 12 \text{ MN}$

b)  $S_1 = -12 \text{ MN}$  (trykstang)

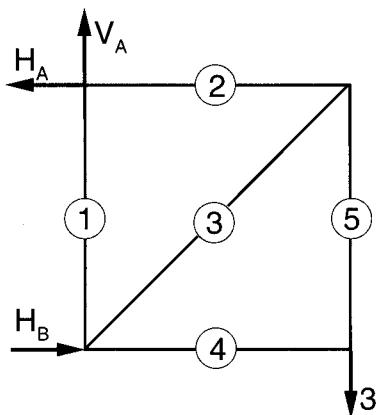
$S_2 = 16,97 \text{ MN}$  (trækstang)

$S_3 = -12 \text{ MN}$  (trykstang)



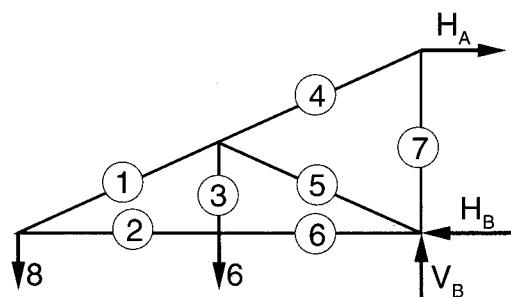
87. a)  $H_A = 3 \text{ MN}$   
 $V_A = 3 \text{ MN}$   
 $H_B = 3 \text{ MN}$

b)  $S_1 = 3 \text{ MN}$  (trækstang)  
 $S_2 = 3 \text{ MN}$  (trækstang)  
 $S_3 = -4,24 \text{ MN}$  (trykstang)  
 $S_4 = 0$   
 $S_5 = 3 \text{ MN}$  (trækstang)



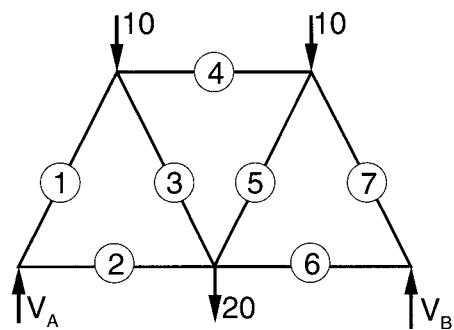
88.  $H_A = 22 \text{ kN}$   
 $H_B = 22 \text{ kN}$   
 $V_B = 14 \text{ kN}$

Stang nr.	Størrelse (kN)	
	Træk	Tryk
1	17,89	
2		16
3	6	
4	24,6	
5		6,71
6		16
7		11



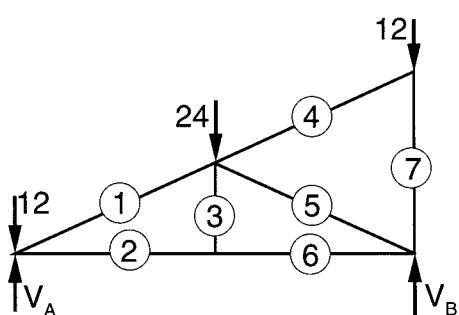
89.

Stang nr.	Størrelse (kN)	
	Træk	Tryk
1 = 7		23,09
3 = 5	11,55	
2 = 6	11,55	
4		17,32



90.

Stang nr.	Størrelse (kN)	
	Træk	Tryk
1		26,83
2	24	
3	0	
4	0	
5		26,83
6	24	
7		12

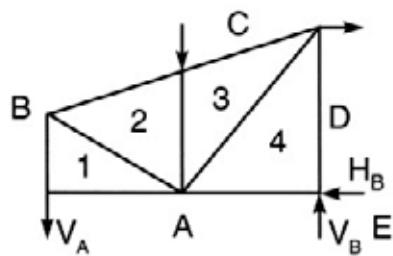


91.

$$V_A = 300 \text{ N}$$

$$V_B = 900 \text{ N}$$

Stang nr.	Størrelse (kN)	
	Træk	Tryk
a-1	0	
b-1	300	
b-2	335	
1-2		335
c-3	335	
2-3		600
a-4		800
d-4		900
3-4	0	

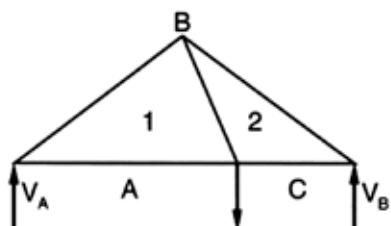


92.

$$V_A = 0,89 \text{ kN}$$

$$V_B = 1,71 \text{ kN}$$

Stang nr.	Størrelse (kN)	
	Træk	Tryk
a-1	1,19	
b-1		1,48
S <sub>1</sub> = b-2		2,85
S <sub>2</sub> = c-2	2,28	
S <sub>3</sub> = 1-2	2,82	



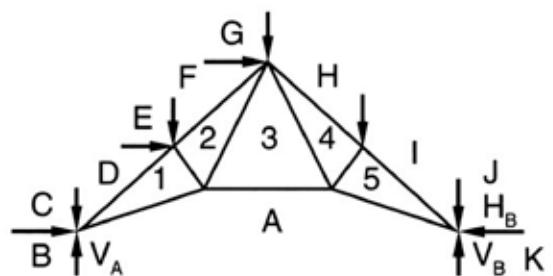
93.

$$V_A = 11,11 \text{ kN}$$

$$V_B = 12,89 \text{ kN}$$

$$H_B = 4 \text{ kN}$$

Stang nr.	Størrelse (kN)	
	Træk	Tryk
S <sub>2</sub> = a-1	13,7	
a-3	5,1	
a-5	12	
S <sub>1</sub> = d-1		18,73
f-2		17
h-4		16,8
i-5		20,7
1-2		5,8
2-3	10,2	
3-4	8,4	
4-5		4,75

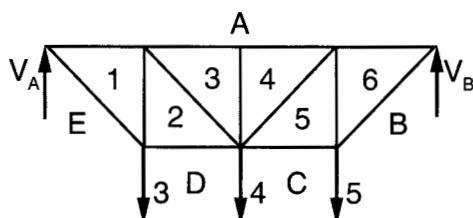


94.

$$V_A = 5,5 \text{ MN}$$

$$V_B = 6,5 \text{ MN}$$

Stang nr.	Størrelse (kN)	
	Træk	Tryk
a-1		5,5
a-3		8
a-4		7,5
a-6		6,5
b-6	9,19	
c-5	6,5	
d-2	5,5	
e-1	7,78	
1-2		2,5
2-3	2,83	
3-4	0	
4-5	2,12	
5-6		1,5



95.

- a)  $F = 2,549 \text{ kN}$  ( $g = 10 \text{ m/sek}^2$ )  
 b)  $H_A = 2,549 \text{ kN}$   
 $H_B = 2,549 \text{ kN}$   
 $V_B = 2,549 \text{ kN}$   
 c)  $S_1 = 3,604 \text{ kN}$  (trækstang)  
 $S_2 = -2,549 \text{ kN}$  (trykstang)  
 $S_3 = -2,549 \text{ kN}$  (trykstang)

## 4. STYRKELÆRENS GRUNDBEGREBER

### Opgave 96-110

Resultaterne er baseret på, at der på de givne figurer er indlagt et koordinatsystem, hvor x-aksen er beliggende i arealets nederste sidelinje, og y-aksen er beliggende i arealets yderste, venstre sidelinje.

96. a)  $(x,y) = (11,43, 25,36)$   
 b)  $v = 37,98^\circ$
97.  $(x,y) = (20, 23,27)$
98.  $(x,y) = (15, 21,67)$
99.  $(x,y) = (60, 75,7)$
100.  $(x,y) = (25, 9,71)$
101.  $(x,y) = (40, 47,89)$
102.  $(x,y) = (51,43, 18,57)$
103.  $(x,y) = (47,5, 45)$
104.  $(x,y) = (14,72, 16,67)$
105.  $(x,y) = (488,32, 162,49)$
106.  $(x,y) = (2, 0,79)$
107.  $(x,y) = (15, 15,17)$
108.  $F_1 = 52 \text{ N}$  (til venstre)  
 $F_2 = 65 \text{ N}$  (til højre) ( $g = 10 \text{ m/s}^2$ )
109. Vinklen =  $25,11^\circ$
110.  $(x,y) = (74,85, 75)$  (x- og y-aksen er placeret i henholdsvis snitpladens nederste kantlinje og venstre kantlinje).
111.  $I_x = 1,152 \cdot 10^6 \text{ mm}^4$        $I_y = 0,879 \cdot 10^6 \text{ mm}^4$
112.  $I_x = I_y = 258 \cdot 10^6 \text{ mm}^4$
113. ( $y = 19,42 \text{ mm}$  - tyngdepunktsafstand fra nederste linje)  
 $I_x = 0,44 \cdot 10^6 \text{ mm}^4$        $I_y = 0,47 \cdot 10^6 \text{ mm}^4$
144. a =  $188,15 \text{ mm}$
115.  $I_x = 22,4 \cdot 10^6 \text{ mm}^4$        $I_y = 4,8 \cdot 10^6 \text{ mm}^4$
116.  $I_x = 38,2 \cdot 10^6 \text{ mm}^4$        $W_x = 382 \cdot 10^3 \text{ mm}^3$   
 $I_y = 16,06 \cdot 10^6 \text{ mm}^4$        $W_y = 160,6 \cdot 10^3 \text{ mm}^3$
117.  $(x,y) = (15,20)$  - koordinatsystemet er indlagt således, at y-aksen er placeret i arealets venstre sidelinje, og x-aksen er placeret i arealets nederste linje.  
 $I_x = 0,04 \cdot 10^6 \text{ mm}^4$        $W_x = 2 \cdot 10^3 \text{ mm}^3$   
 $I_y = 0,085 \cdot 10^6 \text{ mm}^4$        $W_y = 3,4 \cdot 10^3 \text{ mm}^3$

118.  $(x,y) = (19,38, 17,18)$  - koordinatsystemet er indlagt således, at y-aksen er placeret i arealets venstre sidelinje, og x-aksen er placeret i arealets nederste linje.  
 $I_x = 0,1228 \cdot 10^6 \text{ mm}^4$      $W_x = 5,39 \cdot 10^3 \text{ mm}^3$   
 $I_y = 0,0764 \cdot 10^6 \text{ mm}^4$      $W_y = 3,71 \cdot 10^3 \text{ mm}^3$

119.  $y = 106,84 \text{ mm}$  (y er afstanden fra arealets nederste linje til tyngdelinjen)  
 $I_x = 48,24 \cdot 10^6 \text{ mm}^4$      $W_x = 315 \cdot 10^3 \text{ mm}^3$

120.  $y = 94,35 \text{ mm}$  (y er afstanden fra arealets nederste linje til tyngdelinjen)  
 $I_x = 7,29 \cdot 10^6 \text{ mm}^4$      $W_x = 77,31 \cdot 10^3 \text{ mm}^3$

121.  $(x,y) = (13,19)$  - koordinatsystemet er indlagt således, at y-aksen er placeret i arealets venstre sidelinje, og x-aksen er placeret i arealets nederste sidelinje.  
 $I_x = 0,036 \cdot 10^6 \text{ mm}^4$      $W_x = 1,9 \cdot 10^3 \text{ mm}^3$   
 $I_y = 0,072 \cdot 10^6 \text{ mm}^4$      $W_y = 2,7 \cdot 10^3 \text{ mm}^3$

122.  $y = 52,44 \text{ mm}$  (y er afstanden fra arealets nederste linje til tyngdelinjen)  
 $I_x = 7,777 \cdot 10^6 \text{ mm}^4$      $W_x = 148,294 \cdot 10^3 \text{ mm}^3$

123.  $I_x = 2,028 \cdot 10^6 \text{ mm}^4$      $W_x = 50,71 \cdot 10^3 \text{ mm}^3$   
 $I_y = 1,91 \cdot 10^6 \text{ mm}^4$      $W_y = 45,796 \cdot 10^3 \text{ mm}^3$

124. a)  $\sigma = 100 \frac{\text{N}}{\text{mm}^2}$

b)  $\Delta L = 3,8 \text{ mm}$

125. a)  $N = 26950 \text{ N}$   
b)  $\sigma = 77 \frac{\text{N}}{\text{mm}^2}$

126. a)  $N = 11875 \text{ N}$   
b)  $\Delta L = 0,4 \text{ mm}$

127.  $\Delta L = 0,418 \text{ mm}$

## 5. STÅLKONSTRUKTIONER

128.  $22 \cdot 10^3 \text{ N} < 51,27 \cdot 10^3 \text{ N}$

129. a) Rørprofil  $60 \cdot 60 \cdot 2,9 \text{ mm}$   
b)  $135 \cdot 10^3 \text{ N} < 139,93 \cdot 10^3 \text{ N}$

130.  $N_{Ed} = 1160 \text{ kN}$

131. a) Middelsvært gevindrør med  $d = 20 \text{ mm}$   
b)  $40,5 \cdot 10^3 \text{ N} < 43,15 \cdot 10^3 \text{ N}$

132. a)  $S_1 = S_2 = 11,31 \text{ kN}$   
b) Svært gevindrør med  $d = 6 \text{ mm}$   
c)  $11,31 \cdot 10^3 \text{ N} < 13,43 \cdot 10^3 \text{ N}$

133. a)  $19,976 \text{ kN}$  ( $g \sim 10 \frac{\text{m}}{\text{s}^2}$ )

b)  $d = 10,91 \text{ mm} \sim 12 \text{ mm}$

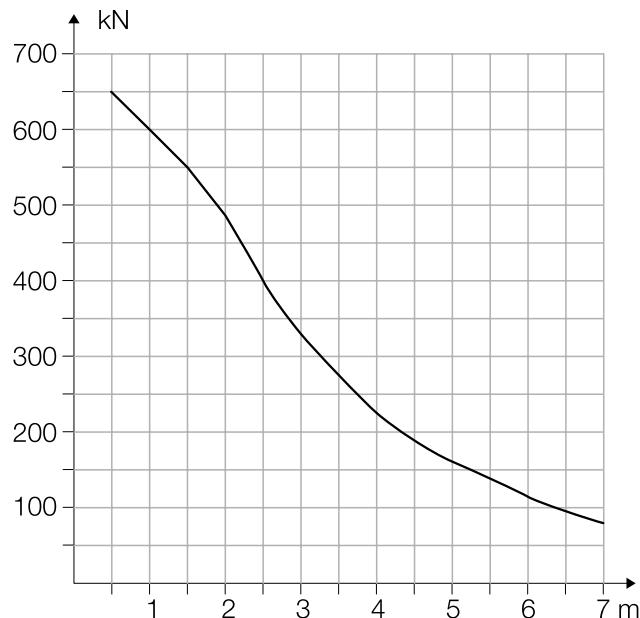
c)  $19,976 \cdot 10^3 \text{ N} < 24,161 \cdot 10^3 \text{ N}$

134. HE 200B :  $520 \cdot 10^3 \text{ N} < 780,024 \cdot 10^3 \text{ N}$

135.  $N_{Ed} \sim 712 \text{ kN}$

136. IPE 240 :  $200 \cdot 10^3 \text{ N} < 222,055 \cdot 10^3 \text{ N}$

137.



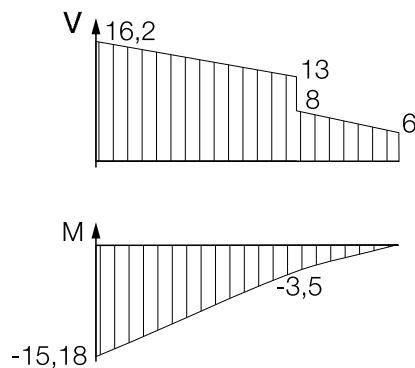
138. HE 140B :  $260 \cdot 10^3 \text{ N} < 395,78 \cdot 10^3 \text{ N}$

139. HE 120B :  $505 \cdot 10^3 \text{ N} < 529,83 \cdot 10^3 \text{ N}$

140.  $N_{Ed} \sim 1029,3 \text{ kN}$

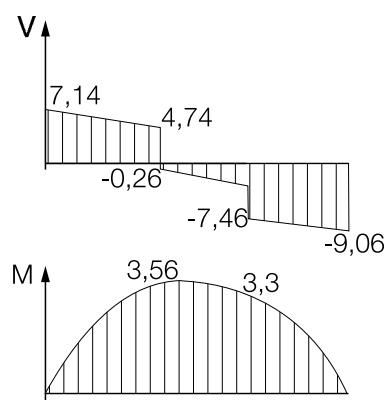
141. a)  $S_1 = 47,67 \text{ kN}$  (trækstang)  
 $S_2 = 62,23 \text{ kN}$  (trykstang)  
b) 1.  $47,67 \cdot 10^3 \text{ N} < 177,53 \cdot 10^3 \text{ N}$   
2.  $62,23 \cdot 10^3 \text{ N} < 156,23 \cdot 10^3 \text{ N}$

142. a)  $V_A = 16,2 \text{ kN}$        $M_A = 15,18 \text{ kNm}$   
b)



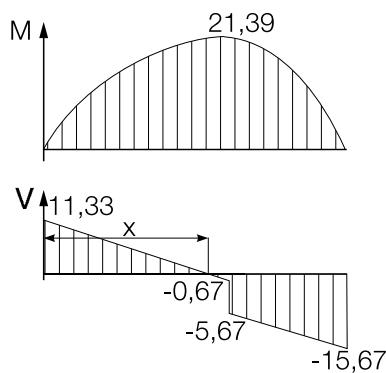
- c) IPE 140  
d)  $15180 \cdot 10^3 \text{ Nmm} < 19325 \cdot 10^3 \text{ Nmm}$

143. a)  $V_A = 7,14 \text{ kN}$        $V_B = 9,06 \text{ kN}$   
b)



- c) INP 80  
d)  $3560 \cdot 10^3 \text{ Nmm} < 4272 \cdot 10^3 \text{ Nmm}$

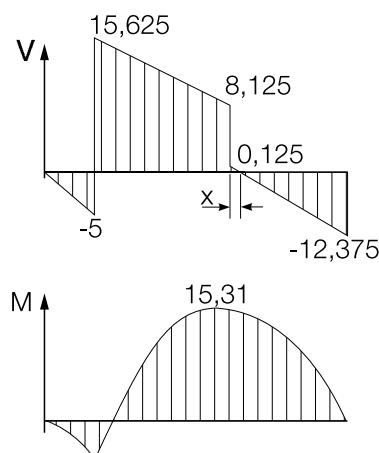
144. a)  $V_A = 11,33 \text{ kN}$        $V_B = 15,67 \text{ kN}$   
b)  $x = 3,78 \text{ m}$  (se figuren)



- c) HE 120B  
d)  $21390 \cdot 10^3 \text{ Nmm} < 30763 \cdot 10^3 \text{ Nmm}$

145.  $q_{\max} = 46,65 \frac{\text{kN}}{\text{m}}$

146. a)  $V_A = 20,625 \text{ kN}$        $V_B = 12,375 \text{ kN}$   
b)  $x = 0,025 \text{ m}$  (se figuren)



- c) INP 140  
d)  $15310 \cdot 10^3 \text{ Nmm} < 16514 \cdot 10^3 \text{ Nmm}$

147. INP 260 ( $I_x = 57,4 \cdot 10^6 \text{ mm}^4 > I = 56,25 \cdot 10^6 \text{ mm}^4$ )

148. HE 200B ( $I_x = 57 \cdot 10^6 \text{ mm}^4 > I = 46,42 \cdot 10^6 \text{ mm}^4$ )

149. a = 371 mm

150. a = 119,35 mm

## 6. TRÆKONSTRUKTIONER

151.  $\sigma_{t,0,d} = 6,8 \text{ MPa} < f_{t,0,d} = 7,99 \text{ MPa}$

152. a) 100 · 200 mm

b)  $\sigma_{t,0,d} = 5,5 \text{ MPa} < f_{t,0,d} = 6,21 \text{ MPa}$

153. a)  $N_{Ed} = 53846,5 \text{ N}$       d)  $N_{Ed} = 80707 \text{ N}$   
 b)  $N_{Ed} = 62799,5 \text{ N}$       e)  $N_{Ed} = 98615 \text{ N}$   
 c)  $N_{Ed} = 71753,5 \text{ N}$

154. a)  $h = 175 \text{ mm} (50 \cdot 175 \text{ mm})$   
 b)  $\sigma_{t,0,d} = 5,33 \text{ MPa} < f_{t,0,d} = 6,21 \text{ MPa}$

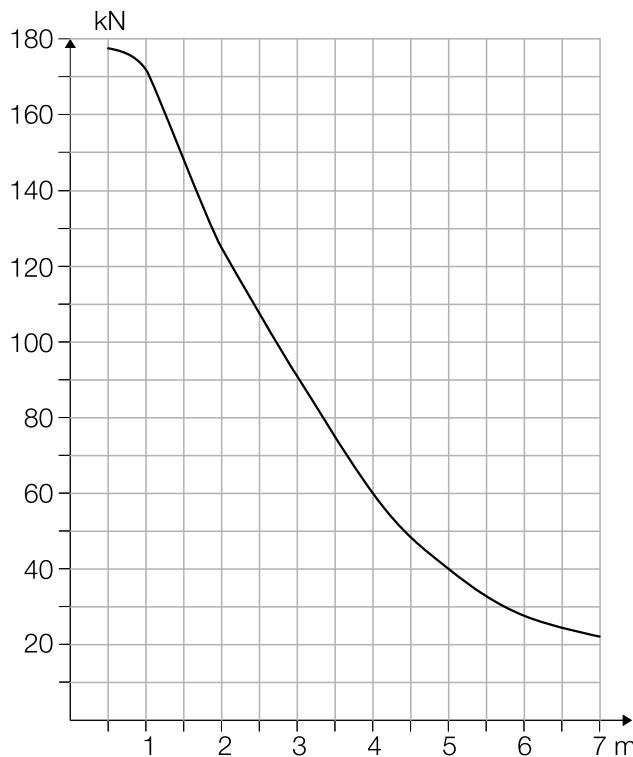
155.  $\sigma_{t,0,d} = 6,67 \text{ MPa} > f_{t,0,d} = 4,88 \text{ MPa}$   
 Omdimensionering: 19 · 175 mm  
 $\sigma_{t,0,d} = 2,86 \text{ MPa} < f_{t,0,d} = 4,88 \text{ MPa}$

156.  $N_{Ed} = 36685 \text{ N}$

157. 150 · 150 mm,  $\sigma_{c,0,d} = 1,87 \text{ MPa} < k_c \cdot k_d \cdot f_{c,0,k} = 3,44 \text{ MPa}$

158.  $N_{Ed} \sim 58275 \text{ N}$

159.



160. 200 · 200 mm

$\sigma_{c,0,d} = 1,5 \text{ MPa} < 3,04 \text{ MPa}$

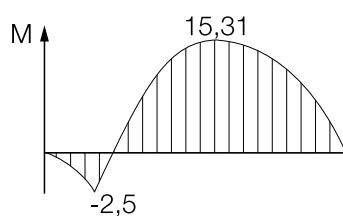
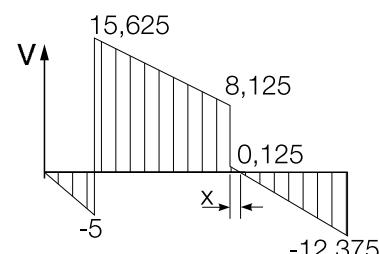
161.  $N_{Ed} \sim 39160 \text{ N}$

162. a) 100 · 225 mm

b)  $\sigma_{m,d} = 5,92 \text{ MPa} < f_{m,d} = 7,99 \text{ MPa}$

163.  $p_{max} = 5,66 \frac{\text{kN}}{\text{m}}$

164. a)  $V_A = 20,625 \text{ kN}$        $V_B = 12,375 \text{ kN}$   
 b)  $x = 0,025 \text{ m}$  (se figuren)



c) 225 · 225 mm

d)  $\sigma_{m,d} = 8,07 \text{ MPa} < f_{m,d} = 10,65 \text{ MPa}$

165.  $u_{max} = 8,33 \text{ mm}$

166. Deformation: 140 · 220 mm

$u = 7,66 \text{ mm} < u_{max} = 8 \text{ mm}$

## 7. MASKINELEMENTER

167. a)  $\sigma = 78 \text{ MPa} < \sigma_{\text{til}} = 85 \text{ MPa}$

$$\tau = 3,25 \text{ MPa} < \tau_{\text{til}} = 65 \text{ MPa}$$

b)  $\sigma = 66,3 \text{ MPa} < \sigma_{\text{til}} = 85 \text{ MPa}$

$$\tau = 2,6 \text{ MPa} < \tau_{\text{til}} = 65 \text{ MPa}$$

168. a) torsion - varierende

b)  $d = 35,39 \text{ mm}$

169. Fladetryk i gaffel:  $p = 27,5 \text{ MPa} < p_{\text{til}} = 50 \text{ MPa}$

Fladetryk i midterstykke:

$$p = 34,5 \text{ MPa} < p_{\text{til}} = 75 \text{ MPa}$$

Forskydning:  $\tau = 17,5 \text{ MPa} < \tau_{\text{til}} = 90 \text{ MPa}$

Bøjning:  $\sigma_b = 34,4 \text{ MPa} < \sigma_{b\text{til}} = 85 \text{ MPa}$

170. a)  $V_A = 57,6 \text{ kN} \quad V_B = 38,4 \text{ kN}$

b)  $M_1 = 2880 \text{ kNm}$

$$M_2 = 10368 \text{ kNm}$$

$$M_3 = 13824 \text{ kNm}$$

$$M_4 = 11904 \text{ kNm}$$

$$M_5 = 1920 \text{ kNm}$$

c)  $d_1 = 69,7 \text{ mm}$

$$d_2 = 106,8 \text{ mm}$$

$$d_3 = 117,6 \text{ mm}$$

$$d_4 = 111,9 \text{ mm}$$

$$d_5 = 60,9 \text{ mm}$$